

A unit cell model of a Regenerative Hydrogen-Vanadium Fuel Cell

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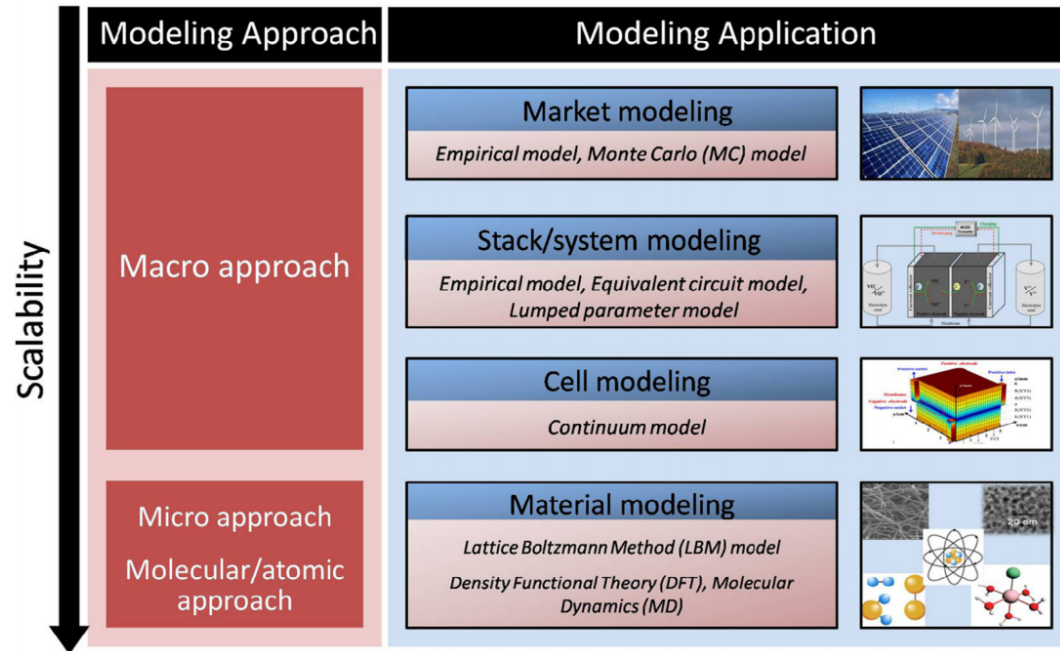


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Content

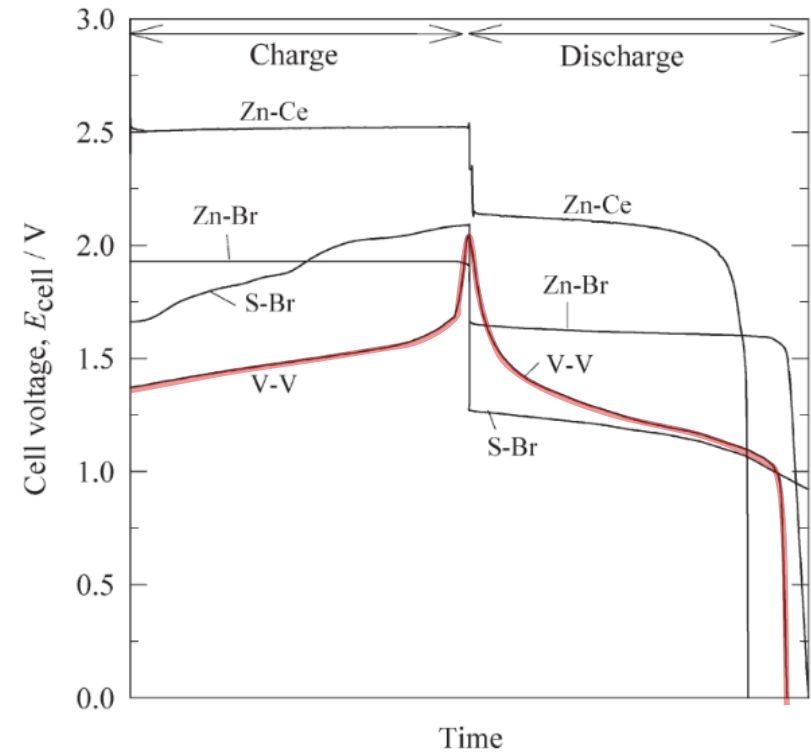
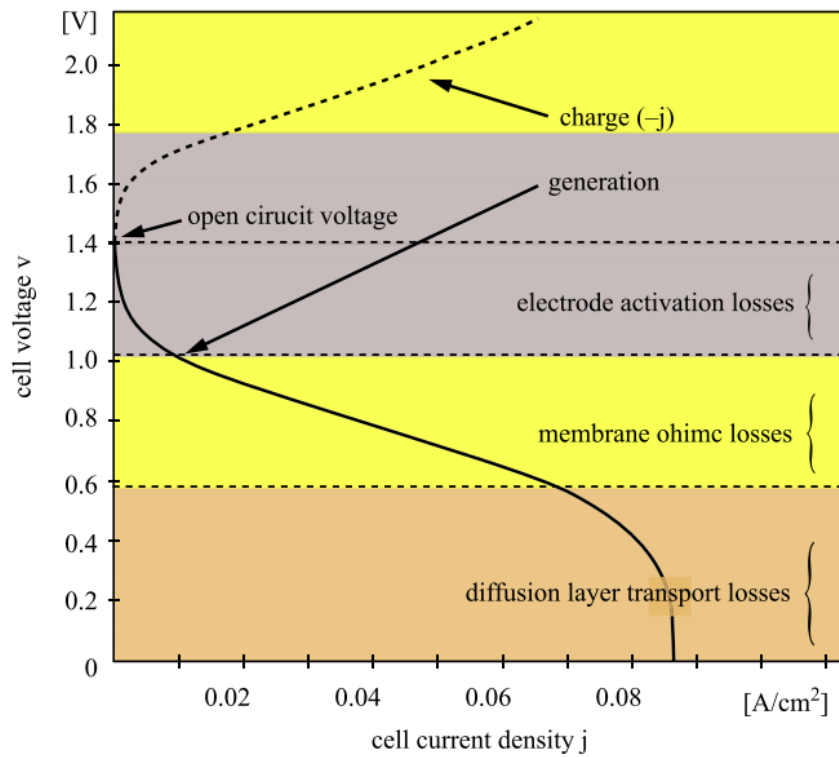
- Introduction
 - Regenerative Hydrogen-Vanadium Fuel Cell (RHVFC)
 - Mathematical model
 - Experimental tests
 - Open circuit potential
 - Model calibration and validation
 - Conclusions and next steps
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Motivation of the study



To develop a mixed model approach that considers a lumped stack/system and cell continuum models and could better explain how the phenomena influence the flow battery performance.

Modeling of RFBs



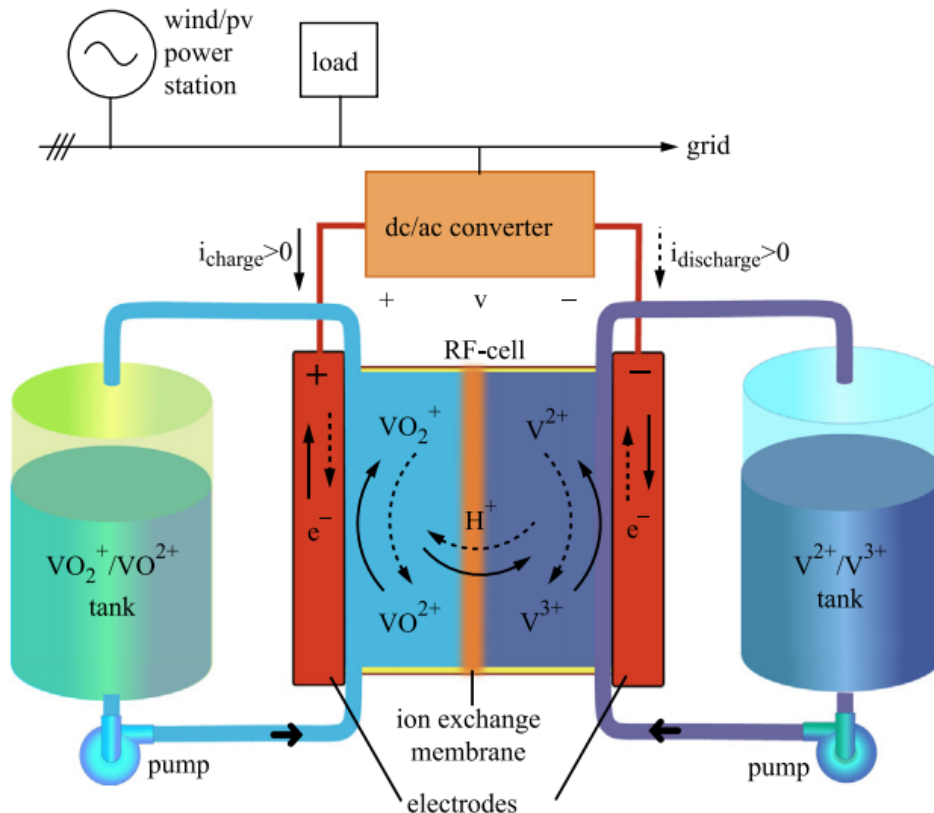
Vanadium redox flow battery

Vanadium based RFB

- Vanadium / halide
 - Vanadium / air
- Anolyte V(II) / V(III)

Hydrogen based RFB

- H₂ / Br₂
- H₂ / Fe
- H₂ / Ce



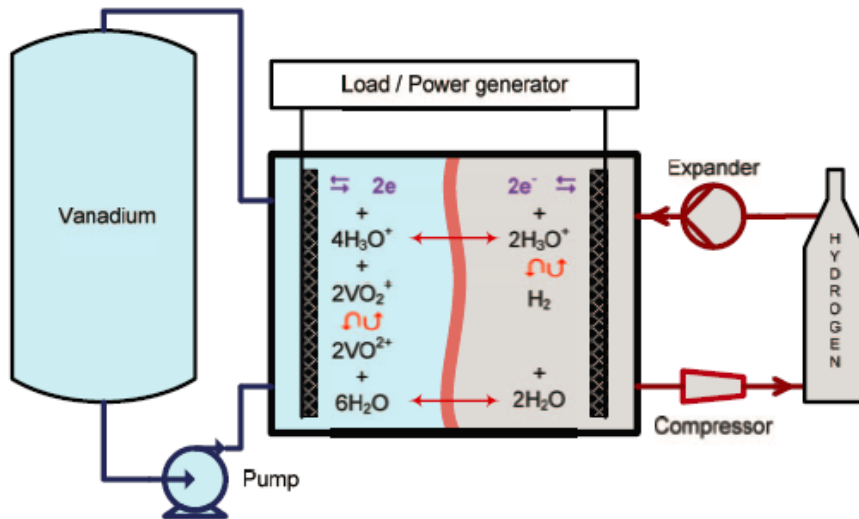
Advantages

- Scalability and flexibility
- Independent sizing of power and energy
- High round-trip efficiency (>80%) and depth of discharge
- Long cycle life (>12000)
- Fast response
- Reduced environmental impact

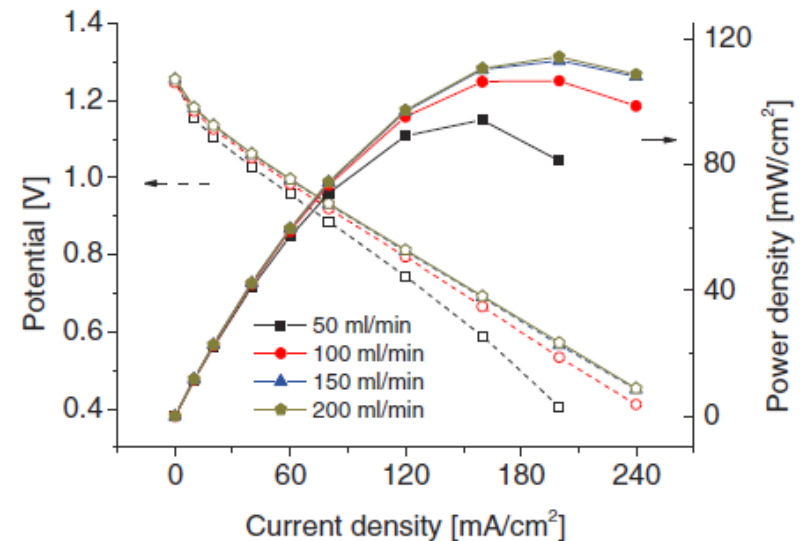
Disadvantages

- Low specific energy density (~30 Wh kg⁻¹)
- Limited operating window (10-40 °C) for vanadium concentration below 2 M.
- Electrode and membrane degradation
- Shunt currents
- High capital cost (\$150-\$1000/kWh)
- Vanadium electrolyte ~40% total cost

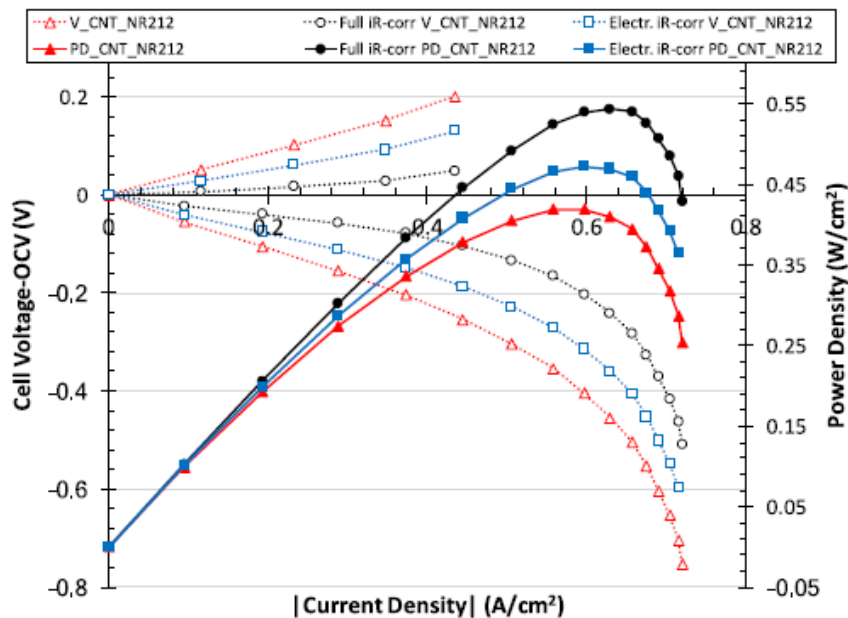
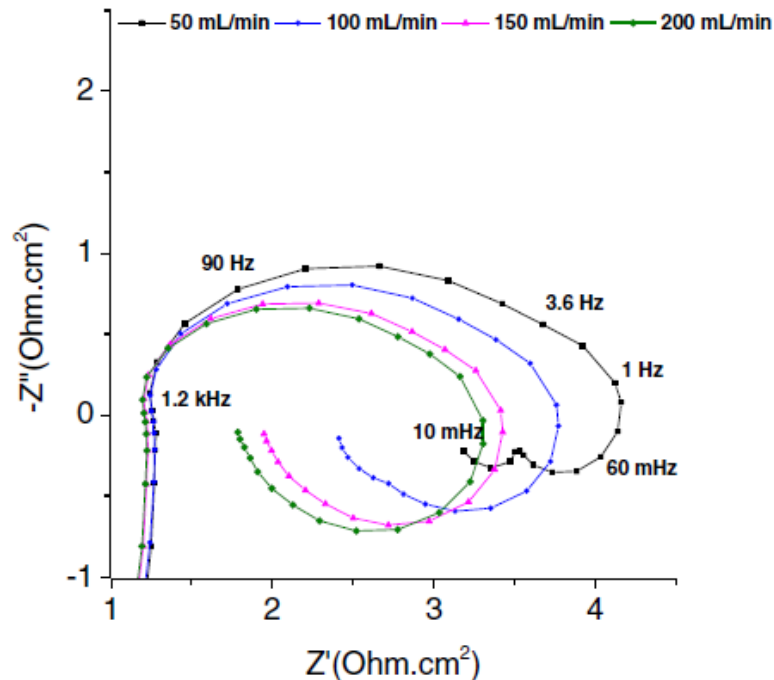
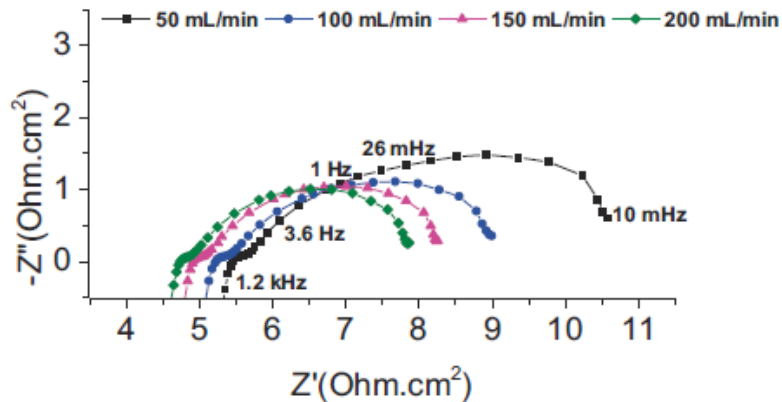
Regenerative Hydrogen-Vanadium Fuel Cell (RHVFC)



- Fast hydrogen kinetics
- Absence of cross-mixing
- Precious metal catalyst – HOR/HER
- Expertise on PEMFCs



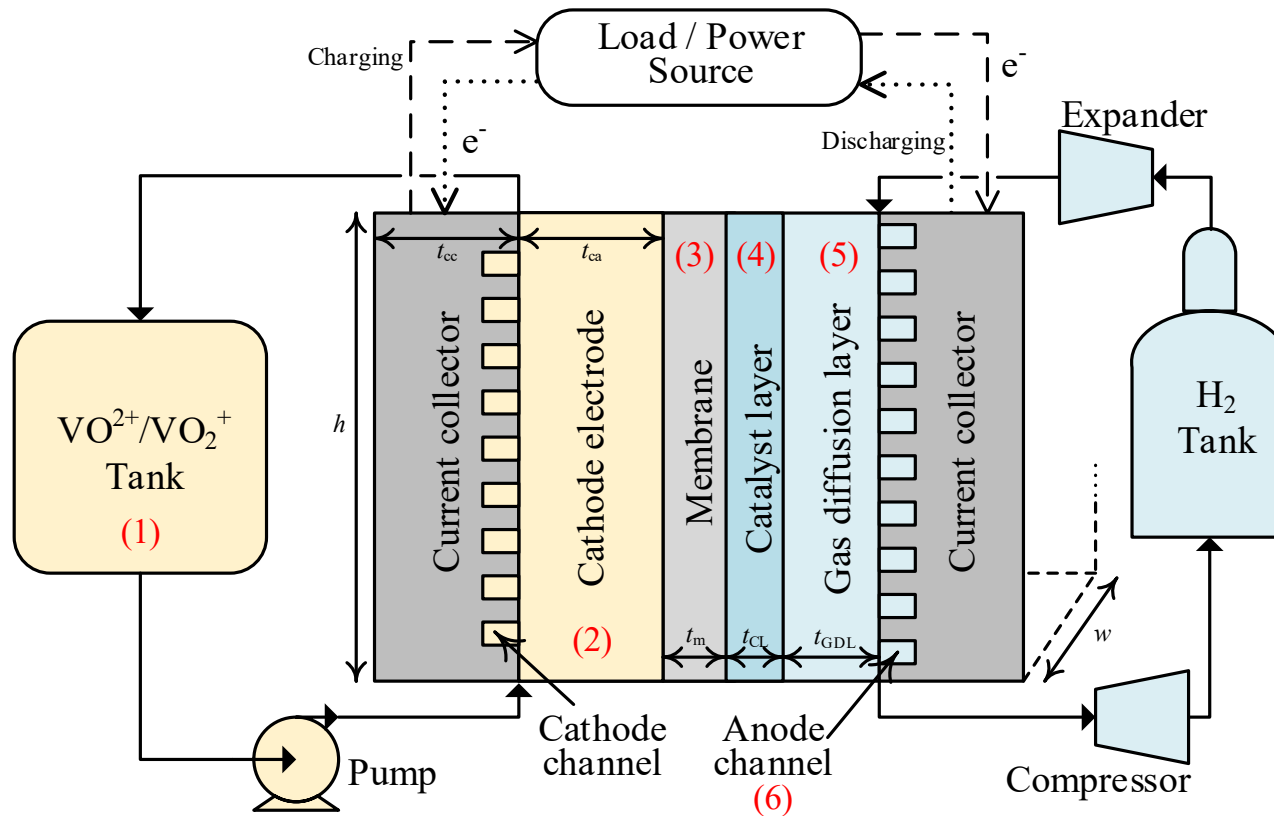
- *Untreated carbon paper*
- *Nafion 117*
- *GDL, 0.5 mg Pt cm⁻²*



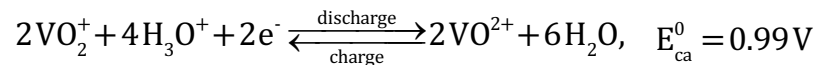
- *Untreated carbon paper*
- *Nafion 117*
- *GDL, 0.5 mg Pt cm⁻²*

- *Carbon nanotube electrode*
- *NR 212*
- *SGL 35 BC GDL, 0.48 mg Pt cm⁻²*

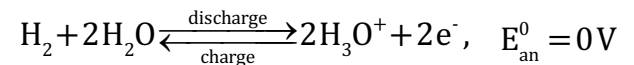
Unit cell model for the RHVFC



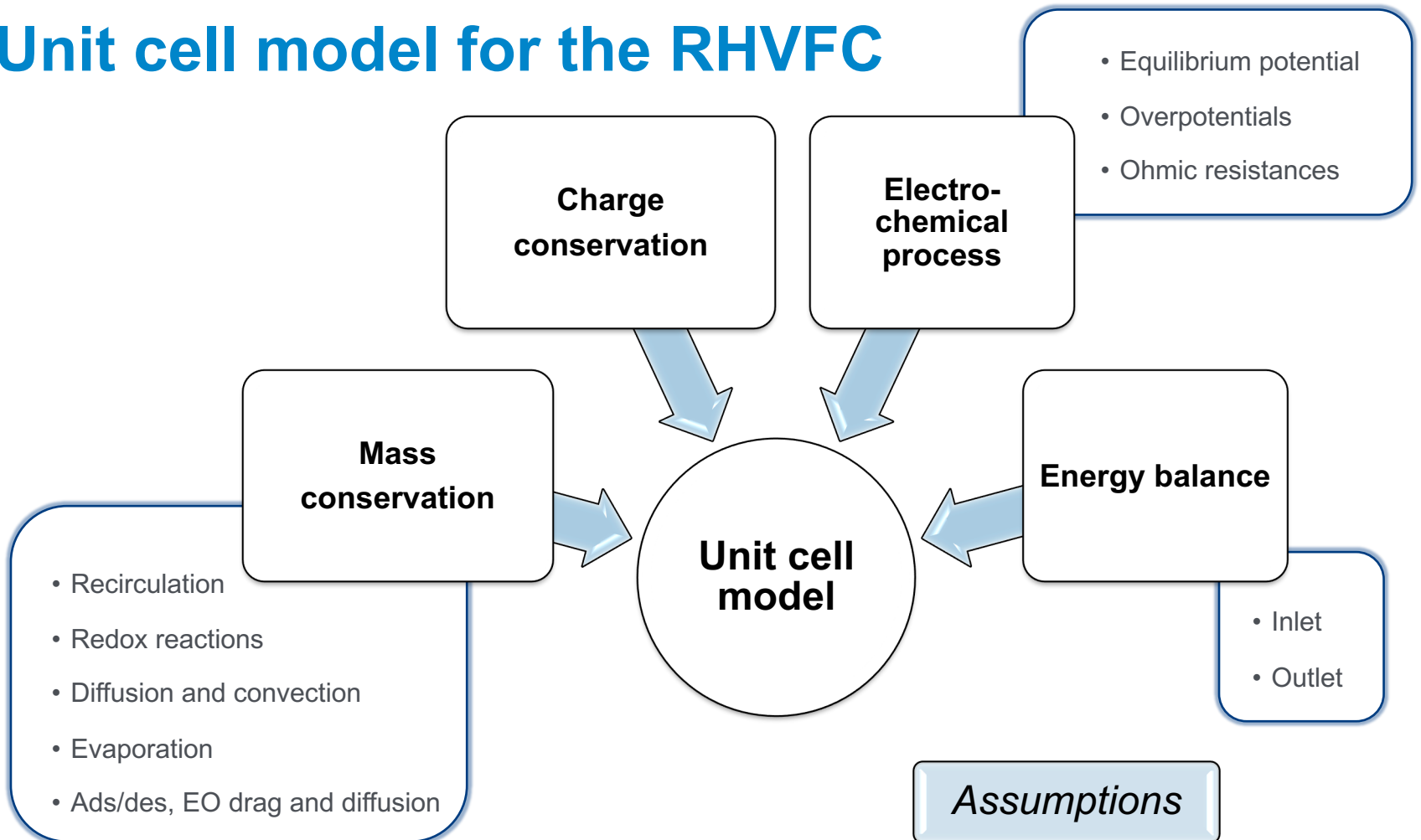
Cathode:



Anode:



Unit cell model for the RHVFC

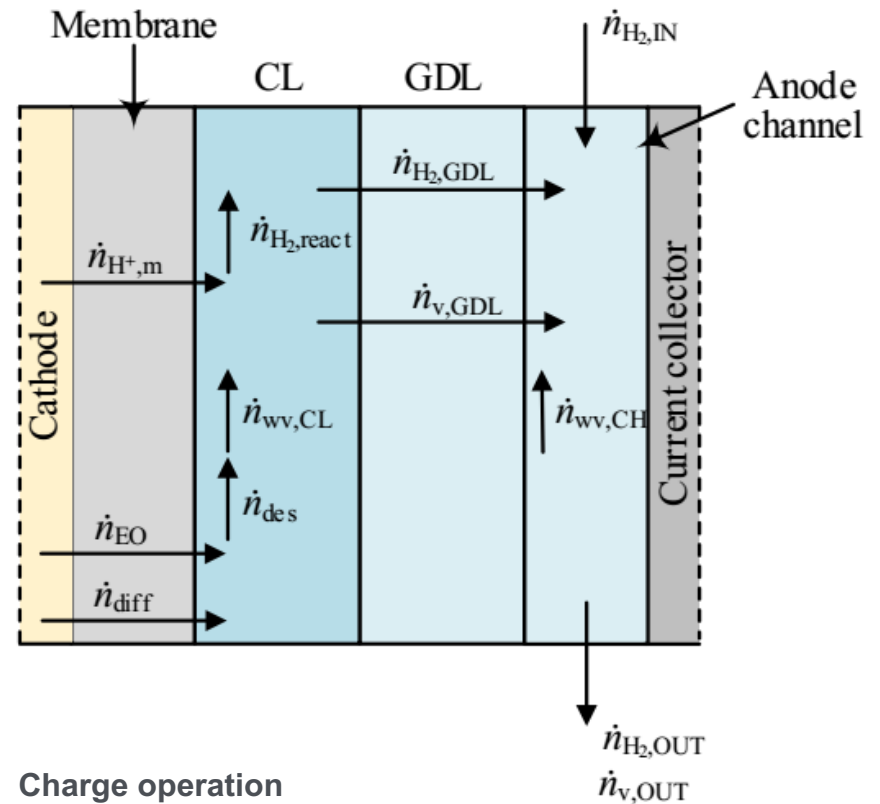


Hydrogen side

Dissolved water transport

Dusty Gas Model

Evaporation/condensation



Anode

$$V_{CL} \varepsilon_{CL} (1 - s_{CL}) \frac{dc_{H_2,CL}}{dt} = \pm \frac{A_{CL} j}{2F} - \dot{n}_{H_2,GDL}$$

Cathode

$$\varepsilon_{ca} V_{ca} \frac{dc_{VO^{2+}}}{dt} = Q_{ca} (c_{VO^{2+},T} - c_{VO^{2+}}) \mp \frac{A_{ca} j}{F}$$

Mass
balances

Electro-
neutrality

Anode

$$c_{H^+} + z_f c_f = 0$$

Cathode

$$\varepsilon_{ca} V_{ca} \left(2 \frac{dc_{VO^{2+}}}{dt} + \frac{dc_{VO_2^+}}{dt} + \frac{dc_{H^+}}{dt} - \frac{dc_{HSO_4^-}}{dt} - 2 \frac{dc_{SO_4^{2-}}}{dt} \right) = 0$$

Open
circuit
potential

Kinetics

$$E_{cell} = E_{OCP} \pm |\eta_{ca}| \pm |\eta_{an}| \pm \eta_{ohm}$$

Cell

$$E_{eq} = E_{cell}^0 + \frac{RT}{F} \ln \left(\frac{c_{V(V)} c_{H^+,ca}^2 P_{H_2}^{0.5} c_{H^+,an}}{c_{V(IV)} c_{H^+,an} c_{H^+,ca}} \cdot \gamma_{OCP} \right)$$

Anode

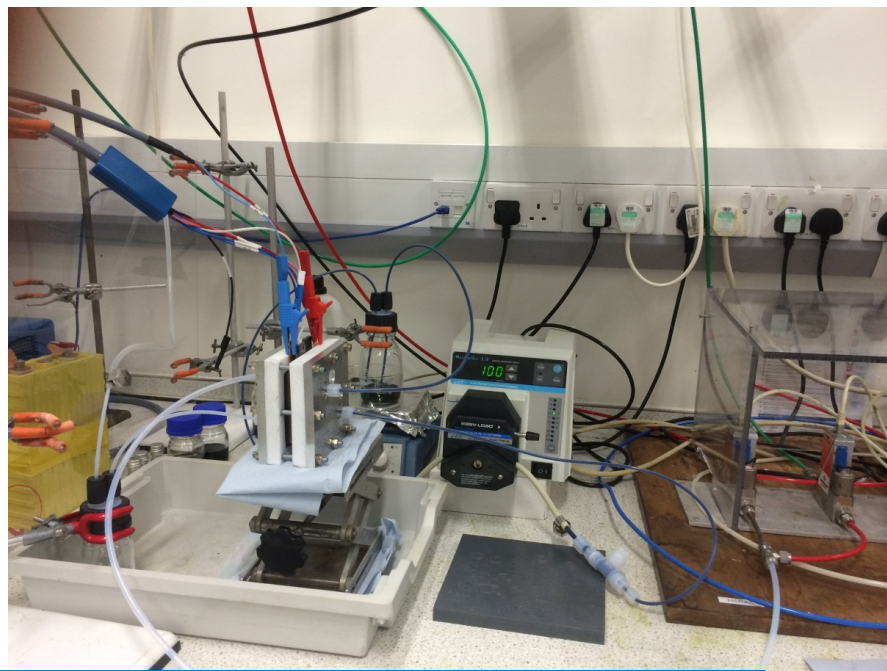
$$\frac{j^{TV}}{k_{des}} = FZ \left(\theta_{H_{ad}}^{TV} \exp \left(\frac{\beta F \eta_{an}}{RT} \right) - B \left(1 - \theta_{H_{ad}}^{TV} \right) \exp \left(\frac{-(1-\beta) F \eta_{an}}{RT} \right) \right)$$

Cathode

$$j^{BV} = j_{0,ca}^{BV} \left[\left(\frac{c_{VO_2^+}^s}{c_{VO_2^+}^b} \right) \left(\frac{c_{H^+}^s}{c_{H^+}^b} \right)^2 \exp \left(\frac{-\alpha F \eta_{ca}}{RT} \right) - \left(\frac{c_{VO^{2+}}^s}{c_{VO^{2+}}^b} \right) \exp \left(\frac{(1-\alpha) F \eta_{ca}}{RT} \right) \right]$$

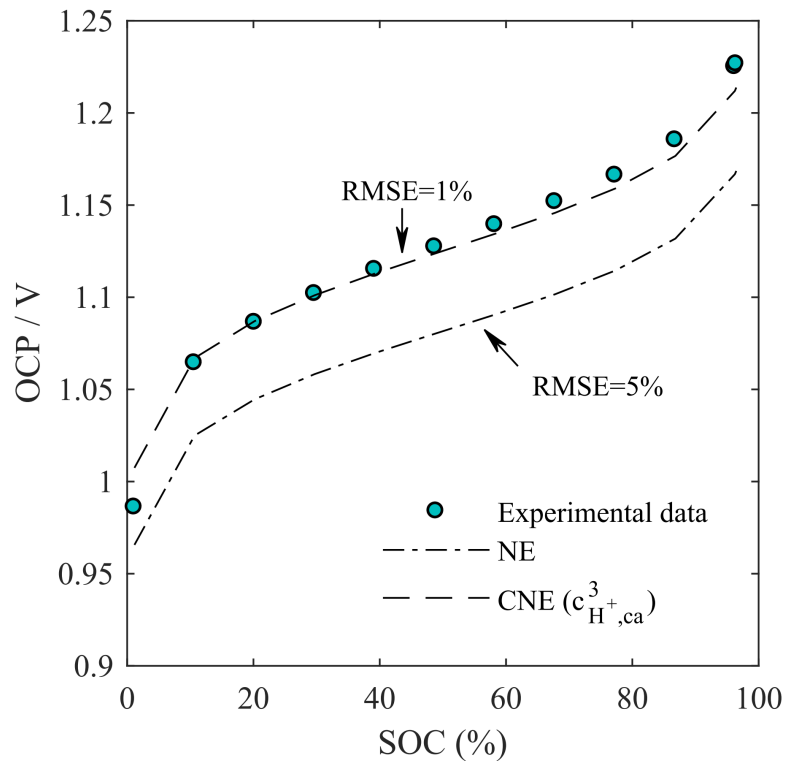
Experimental tests

- $1M\ VOSO_4$
- $60\ mL, 5M\ H_2SO_4$



N°	Test	Current density $A\ m^{-2}$	Catholyte flow rate $mL\ min^{-1}$	Hydrogen flow rate $mL\ min^{-1}$	Cu current collector Yes or No
1	OCP	0	100	100	No
2	Charge-discharge	50	100	100	No
3	Charge-discharge	100	100	100	No
4	Charge-discharge	80	100	100	Yes
5	Charge-discharge	400	100	100	Yes
6	Charge-discharge	400	100	50	Yes
7	Charge-discharge	400	150	100	Yes
8	Charge-discharge	600	100	100	Yes

Open Circuit Potential



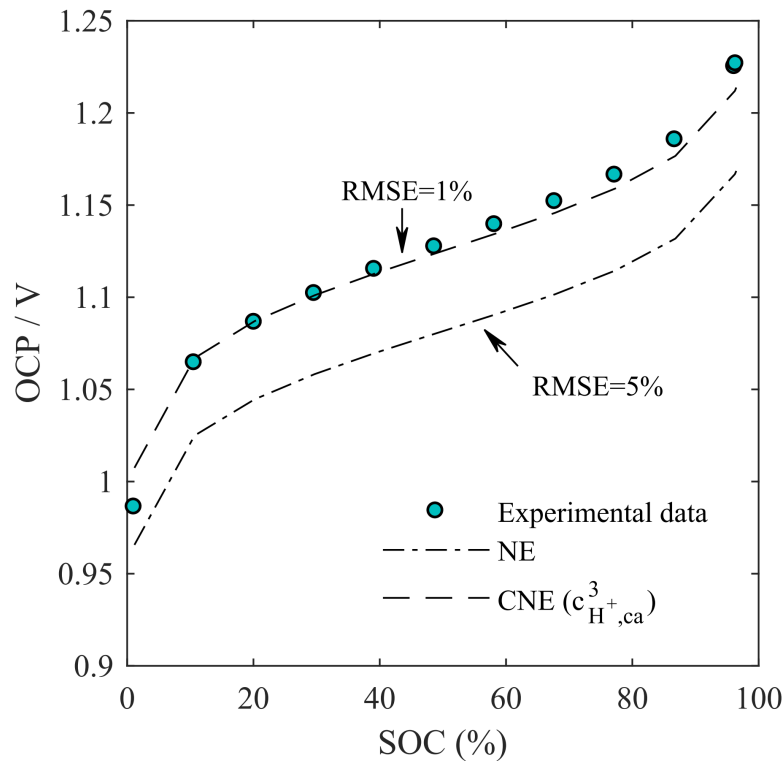
Nernst Equation (NE)

$$E_{OCP} = E_{cell}^0 + \frac{RT}{F} \ln \left(\frac{c_{V(V)} c_{H^+,ca}^2 p_{H_2}^{0.5}}{c_{V(IV)} c_{H^+,an}} \right)$$

Complete Nernst Equation (CNE)

$$E_{OCP} = E_{cell}^0 + \frac{RT}{F} \ln \left(\frac{c_{V(V)} c_{H^+,ca}^2 p_{H_2}^{0.5} c_{H^+,ca}}{c_{V(IV)} c_{H^+,an} c_{H^+,an}} \right)$$

Open Circuit Potential



Nernst Equation (NE)

$$E_{OCP} = E_{cell}^0 + \frac{RT}{F} \ln \left(\frac{c_{V(V)} c_{H^+,ca}^2 p_{H_2}^{0.5}}{c_{V(IV)} c_{H^+,an}} \right)$$

Complete Nernst Equation (CNE)

$$E_{OCP} = E_{cell}^0 + \frac{RT}{F} \ln \left(\frac{c_{V(V)} c_{H^+,ca}^2 p_{H_2}^{0.5} c_{H^+,ca}}{c_{V(IV)} c_{H^+,an} c_{H^+,an}} \right)$$

*Donnan potential
across the membrane*

$$E_m = \frac{RT}{F} \ln \left(\frac{c_{H^+,ca}}{c_{H^+,an}} \right)$$

*Inconsistent with
thermodynamics*

Complete Nernst Equation

Nernst equation

$$E_{OCF} = E_{cell}^0 + \frac{RT}{F} \ln \left(\frac{c_{V(V)} c_{H^+,ca}^2 p_{H_2}^{0.5} c_{H^+,an}}{c_{V(IV)} c_{H^+,an} c_{H^+,ca}} \right)$$

Thermodynamic derivation

*Potential difference
between electrolytes*

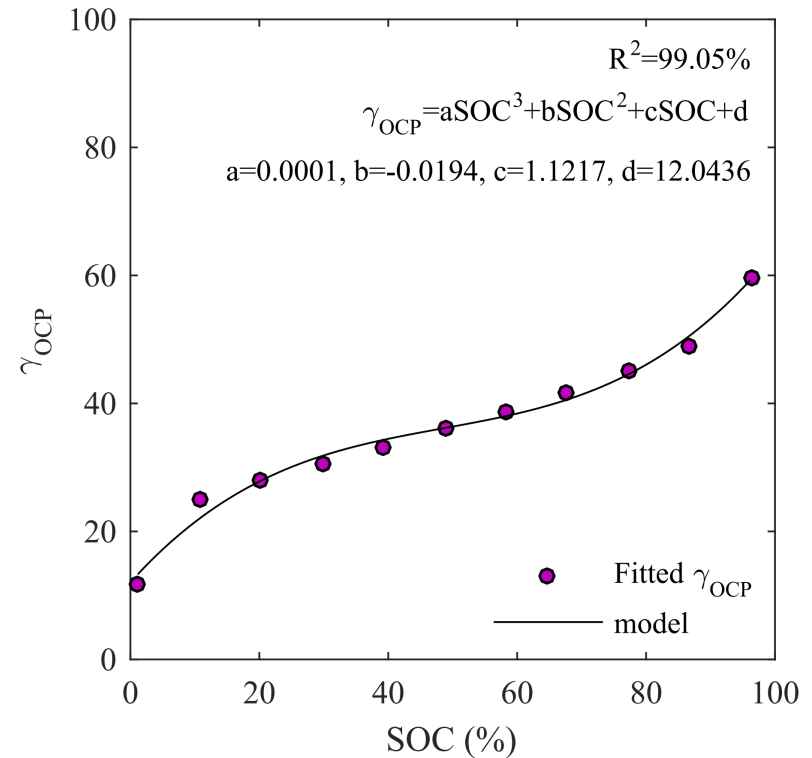
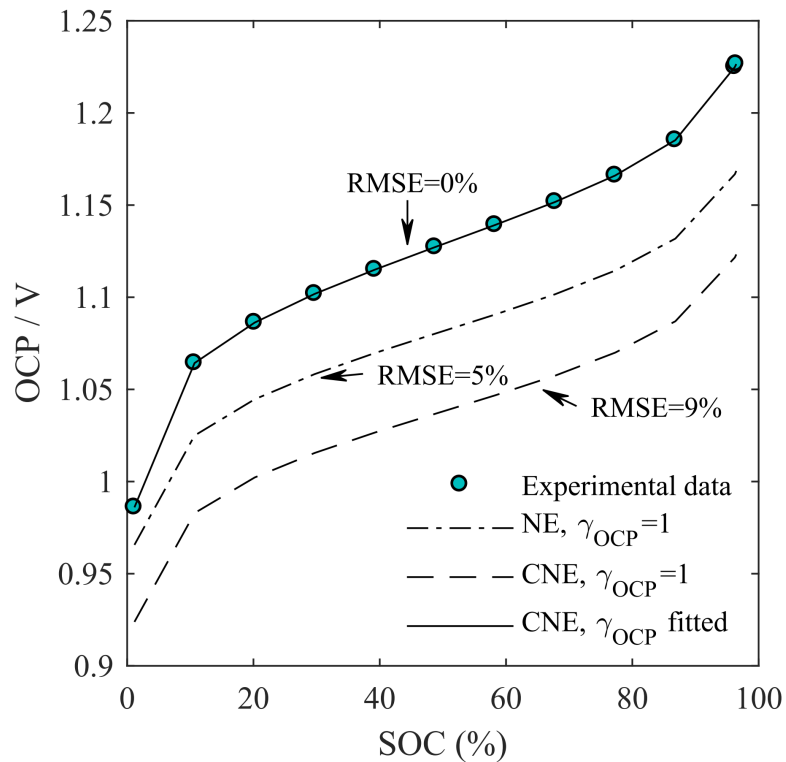
$$\tilde{\mu}_i^\alpha = \mu_i^\alpha + z_i F \phi^\alpha, \quad \tilde{\mu}_{H^+}^e = \tilde{\mu}_{H^+}^m, \quad \rightarrow \quad \phi^{ca} - \phi^{an} = \frac{RT}{F} \ln \left(\frac{c_{H^+,an}}{c_{H^+,ca}} \right)$$

*Donnan potential
across both interfaces*

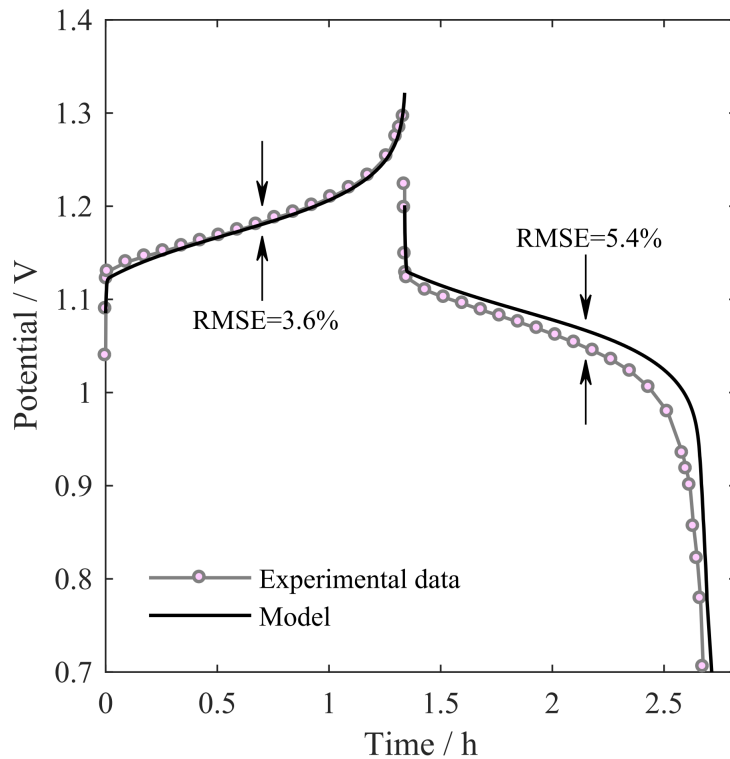
Open Circuit Potential

Thermodynamic derivation of CNE

$$E_{OCP} = E_{cell}^0 + \frac{RT}{F} \ln \left(\frac{c_{V(V)} c_{H^+,ca}^2 p_{H_2}^{0.5} c_{H^+,an}}{c_{V(IV)} c_{H^+,an} c_{H^+,ca}} \gamma_{OCP} \right)$$



Model calibration



$j = 400 \text{ A m}^{-2}$, $Q_V = Q_{H_2} = 100 \text{ mL min}^{-1}$

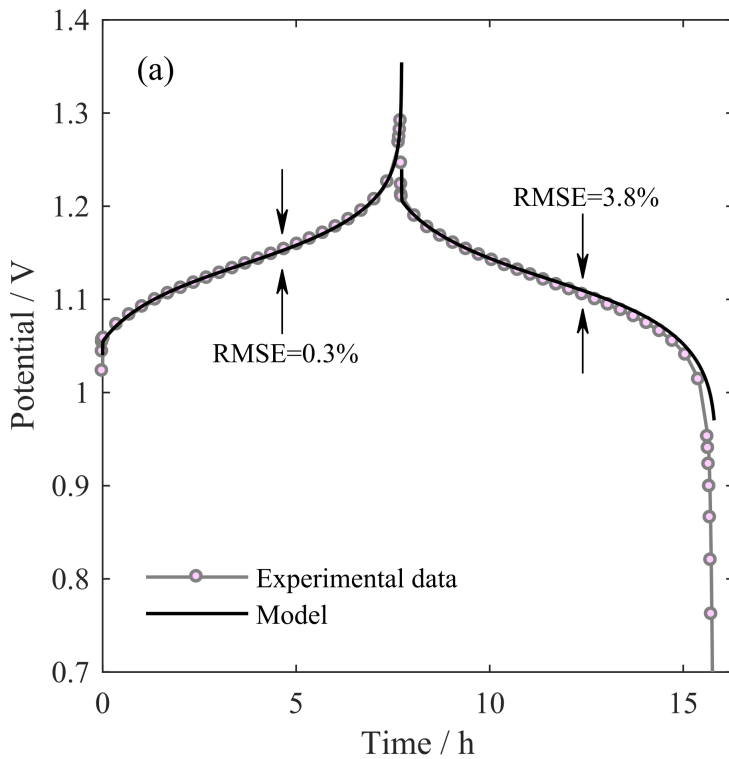
Model implementation

- *MATLAB*
- `ode15s` → solve ODE problem
- `lsqcurvefit` → curve fitting

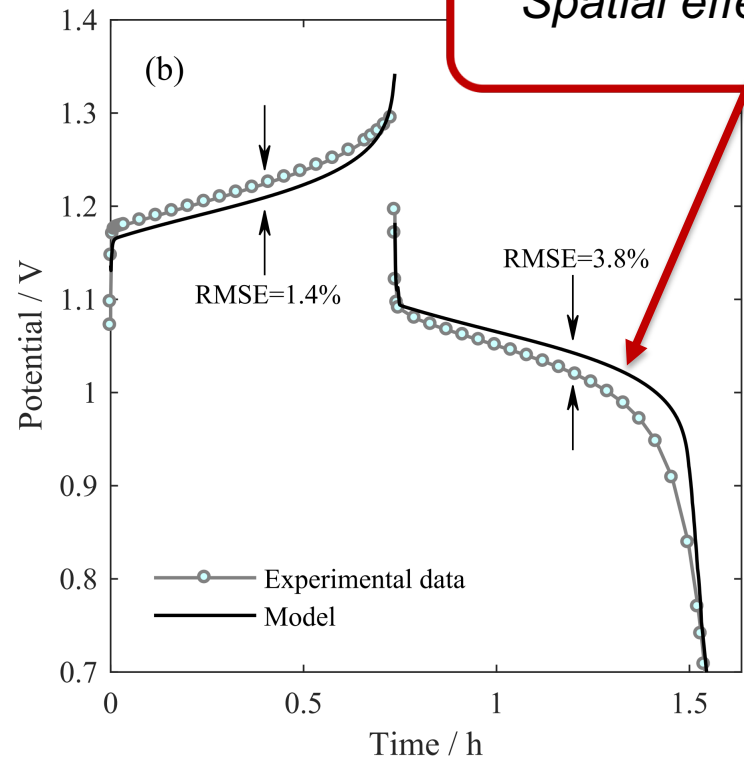
Fitting parameters

- $k_{ca,ref} = 1.2 \times 10^{-7} \text{ m s}^{-1}$
- $\delta = 84.8 \times 10^{-6} \text{ m}$
- $R_C = 0.3 \text{ } \Omega \text{ cm}^2$

Model validation: vary current density

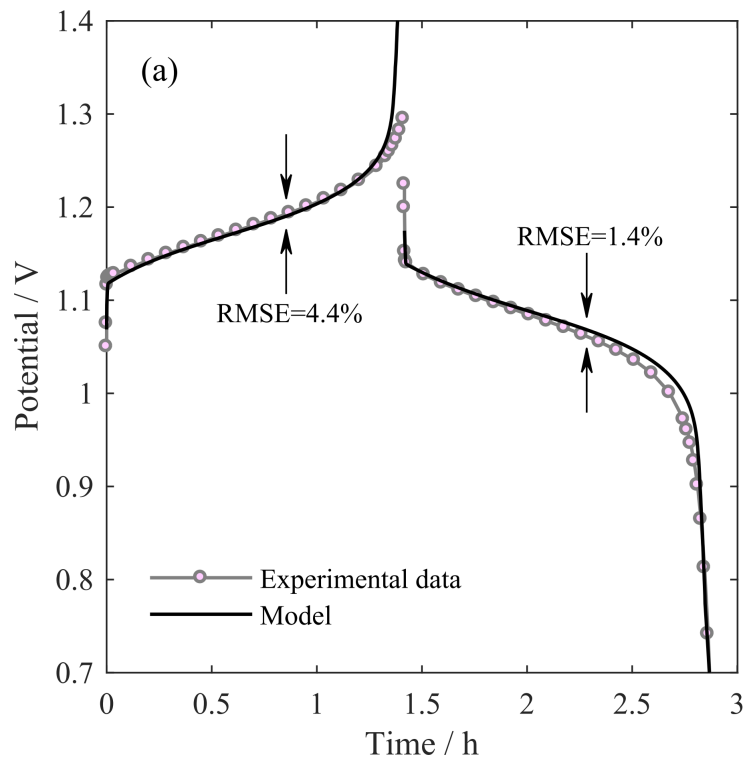


$j = 80 \text{ A m}^{-2}$, $Q_V = Q_{H_2} = 100 \text{ mL min}^{-1}$

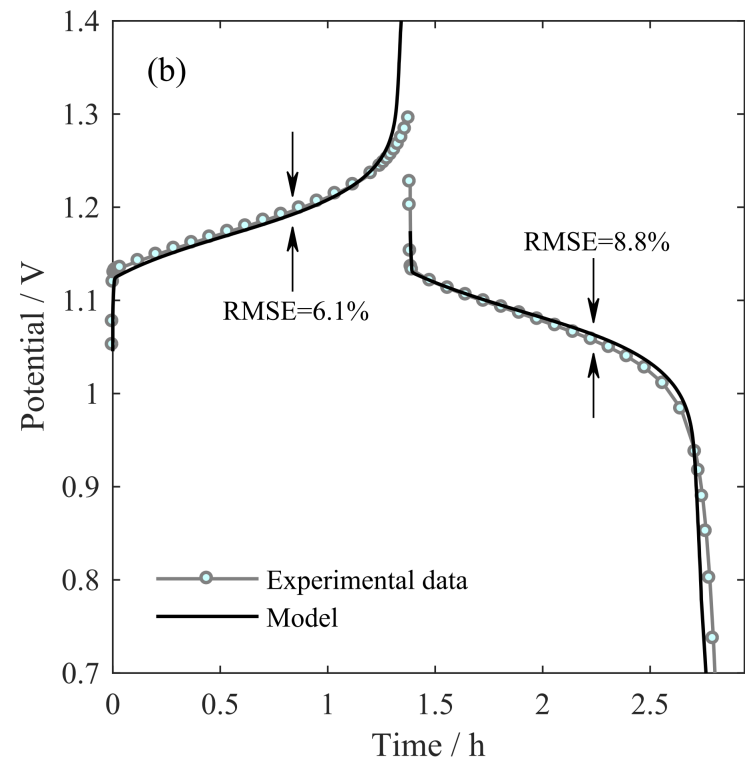


$j = 600 \text{ A m}^{-2}$, $Q_V = Q_{H_2} = 100 \text{ mL min}^{-1}$

Model validation: vary flow rate



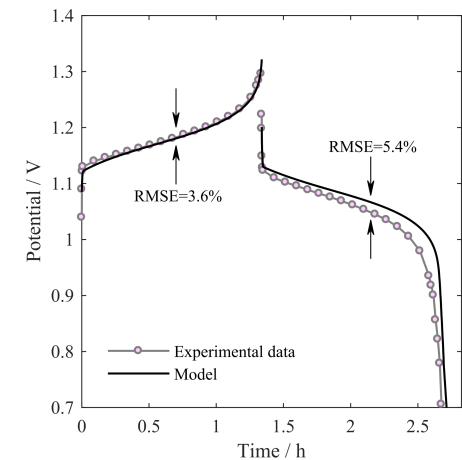
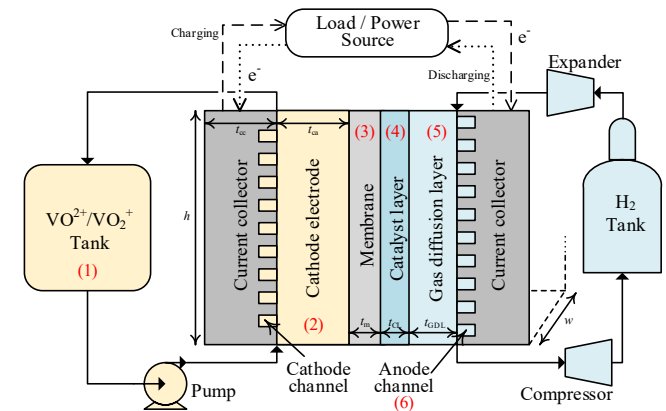
$j = 400 \text{ A m}^{-2}$, $Q_V = 150 \text{ mL min}^{-1}$, $Q_{H_2} = 100 \text{ mL min}^{-1}$



$j = 400 \text{ A m}^{-2}$, $Q_V = 100 \text{ mL min}^{-1}$, $Q_{H_2} = 50 \text{ mL min}^{-1}$

Conclusions

- A unit cell model for a RHVFC was introduced and calibrated against experimental data.
- Model validation at different current densities and flow rates.
- A CNE based on thermodynamic principles was proposed and fit to the OCP data, enabling a global activity coefficient to be obtained.

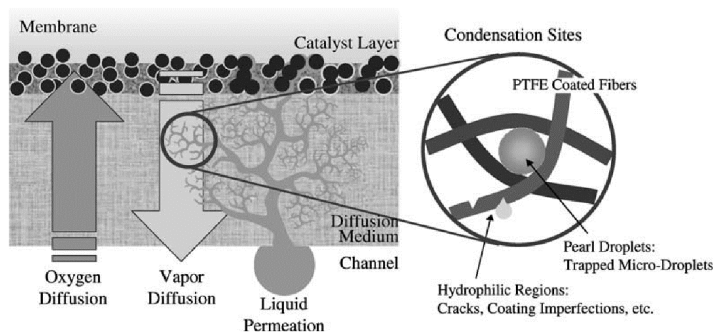


Thermodynamic derivation

$$E_{OCP} = E_{cell}^0 + \frac{RT}{F} \ln \left(\frac{c_{V(V)} c_{H^+,ca}^2 p_{H_2}^{0.5} c_{H^+,an}}{c_{V(IV)} c_{H^+,an} c_{H^+,ca}} \cdot \gamma_{OCP} \right)$$

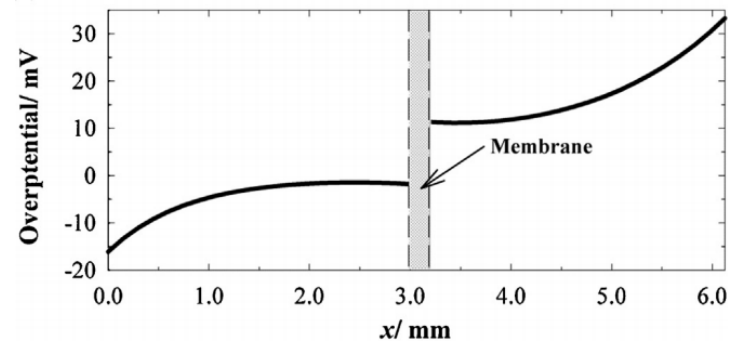
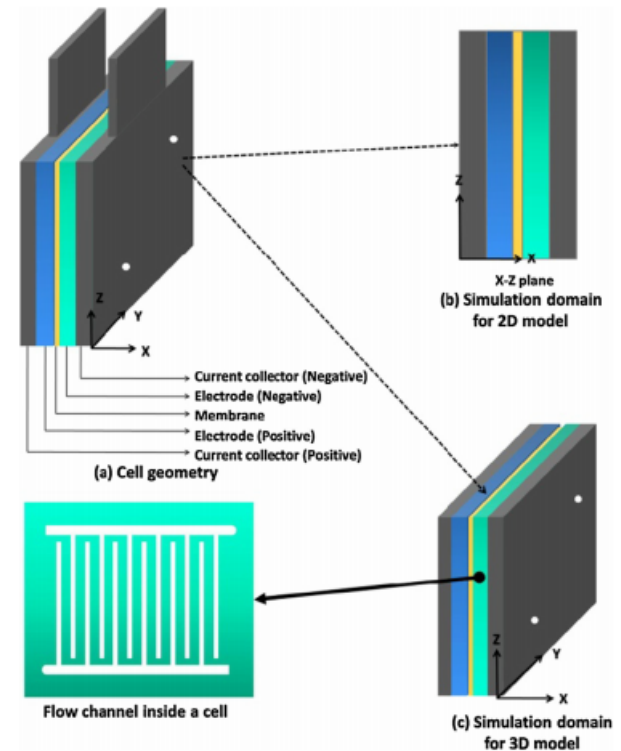
Next steps

- Water transport in GDL



- Cross-over of ionic species
- Experimental data for the RHVFC

- Continuum model (1-2D).



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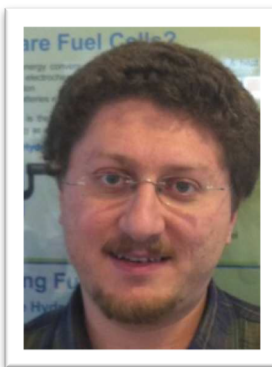
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